

Patent Application of
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SPECIFICATION

TITLE OF THE INVENTION

Method for Forming Particulate Materials

CROSS-REFERENCE OF RELATED APPLICATIONS

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STATEMENT REGARDING FEDERALLY SPONSORED RESEARCH OR DEVELOPMENT

This invention was made with Government support under Grant No. DE-FG03-96ER82300 awarded by the Department of Energy. The Government has certain rights in this invention.

BACKGROUND OF THE INVENTION

The present invention generally relates to the formation of materials useful for electronic applications, in particular for photovoltaic solar cells.

Manufacturers of electronic devices, in particular photoelectronic devices and more specifically photovoltaic devices, are increasingly employing non-elemental materials such as III-V, II-VI and I-III-VI semiconductors and alloys, mixtures and layered structures of such materials. The constituent layers in such photoelectronic devices are typically fabricated using vapor phase deposition processes such as vacuum evaporation,

sputtering and chemical vapor deposition. Vapor phase processes are useful for small-scale research and for high-precision processing of high-value, small-area devices such as integrated circuits. Vapor phase processes have yielded solar cells with high sunlight-to-electricity conversion efficiencies; but it is difficult to deposit uniform films on large areas using coincident vapor phase processes in which the constituent elements are co-deposited, hence coincident vapor phase processes are typically costly to scale up to large device sizes with the control and through-put required for commercial production.

Various researchers have explored sequential vapor phase processes. CuInSe_2 films are typically formed by sequentially depositing solid layers of Cu and In elemental metals and subsequently reacting the Cu-In composite layers with a source of Se to form CuInSe_2 . By solid layer we mean a substantially solid layer of material with minimal included void space. Multi-step, sequential processes substitute separate sequential deposition of constituents in place of co-deposition of constituents, with the intent of mitigating materials interactions that typically complicate co-deposition processes. However, this separation into sequential depositions of different constituents can introduce new complications; for example, vapor phase deposited indium tends to de-wet, forming localized islands, and solid layers of Cu-In alloys can segregate into In-rich and Cu-rich phases when heated, with the result that extreme care is required to maintain the desired planar Cu-In layer structure and lateral composition uniformity during the early stages of subsequent reactions to form CuInSe_2 .

Various researchers have explored techniques for stabilizing metal precursor layers such as Cu-In for CuInSe_2 against de-wetting and phase segregation. For example, thin layers of a chalcogenide metal such as tellurium can be deposited on the substrate prior to the deposition of Cu and In in order to form telluride compounds that mitigate indium de-wetting and phase segregation, and solid layers of binary chalcogenide compounds such as Cu_2Se and In_2Se_3 can be deposited and subsequently interdiffused to form ternary CuInSe_2 . Such processes use chalcogenide compounds to stabilize the primary non-chalcogen constituent metals Cu and In against phase segregation during deposition and subsequent processing.

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Other researchers have explored vapor phase processing of oxide-containing phase-stabilized precursors and mixtures of such precursors with elemental metals and non-oxide chalcogenides. For example, chalcogenide solid films can be formed by depositing a metal oxide solid film and annealing the oxide film in a gas or vapor containing a metal chalcogen such as S, Se, Te or a mixture thereof. Such processes can also utilize layers of single-phase oxide particulates, such as $\text{Cu}_2\text{In}_2\text{O}_5$ particles or such as Cu_2O particles mixed with In_2O_3 particles, and can also utilize solid layers of a mixture of metal and oxide, selenide or sulfide compound constituents. While mitigating certain complications of sequential processes, these phase-stabilized precursor improvements leave unresolved the inherent complexities of achieving the constituent layer uniformity necessary to achieve high-quality semiconductor films using vapor phase processes.

Various researchers have explored alternatives to vapor phase processes for fabricating semiconductor materials for various photoelectronic applications. Electrodeposition can be used to sequentially deposit solid layers of constituent metals such as Cu and In that are subsequently reacted with chalcogenide metals such as Se to form compound semiconductor films. The chalcogenide metal can be embedded in the electroplated solid metal layers by adding Se particles to the electroplating bath so as to incorporate Se particles into one or more of the metallic layers. Additional Se can be added by screen printing a solid Se layer on the Cu-In-Se precursor layers, or by annealing the electrodeposited layers in Se vapor. While avoiding some of the disadvantages of vapor phase processes, such electrodeposition processes are plagued with the challenges of uniform high-rate electrodeposition on large-area substrates and introduce electrodeposition-specific complications such as metal-contaminated waste treatment, recovery and disposal.

Other researchers have explored alternatives to both vapor phase and electrodeposition processes. For example, spray pyrolysis techniques can be used to deposit metal oxide solid layers, and the oxide layers can subsequently be annealed in chalcogenide metal vapor to convert the oxide layers to chalcogenide films. Spray pyrolysis is convenient for depositing multi-component oxides on large areas; but the

materials use efficiencies of spray pyrolysis processes are generally low, hence manufacturing materials costs are generally high.

Alternatively, one can form precursor layers by screen printing a paste of particles or by painting a substrate with a slurry of particles. For example, one can form a Cu-In-Se powder, prepare a paste from the powder, screen print layers of the paste, and anneal the layers to form CuInSe_2 films. Cu-In-Se powders prepared by ball milling or grinding reportedly yield median particle diameters of $1.5 \mu\text{m}$ and larger. Median powder particle diameter determines minimum pinhole-free CuInSe_2 layer thickness; particle diameters of $1.5 - 2 \mu\text{m}$ typically limit CuInSe_2 film thickness to $5 \mu\text{m}$ or greater. Such film thickness are a factor of 5 - 10 thicker than necessary to absorb incident sunlight, and result in high manufacturing materials costs. Researchers preparing CuInSe_2 films by screen printing and sintering CuInSe_2 -based pastes report taking particular measures to avoid the formation of indium oxides deleterious to the CuInSe_2 film properties. Screen-printed films are typically much thicker than required to absorb sunlight sufficiently. Screen printing and related film formation processes are unlikely to be economic unless effective strategies for forming powders with smaller particle diameters and for processing the powders to achieve good film quality are developed.

Various researchers have investigated small particles with median particle diameters of 100 nm and less as a pathway to preparing thin-film materials. Nanoparticles of a wide range of oxides (e.g. ZnO , SnO_2 , WO_3 , etc.) and chalcogenides (e.g. CdS , CdTe , etc.) have been reported, and thin films have been formed from nanoparticles by a variety of techniques. Such small particles can be deposited as particulate layers by a variety of processes including, for example, electrophoresis of colloidal suspensions and slurry spraying. CuInSe_2 films have been prepared by spraying slurries of mixtures of single-phase, binary selenide nanoparticles such as Cu_xSe and In_xSe , but film quality and device performance are poor due to insufficient interparticle diffusion. This implies that small median chalcogenide particle diameters alone do not provide improved particle-based thin film properties.

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The use of an effective flux is known to be particularly important for promoting particle coalescence and grain growth in particle-based thin films. CdCl_2 works well as a flux with Cd-based chalcogenide materials such as CdTe and $\text{Cd}(\text{Se}, \text{Te})$. A comparable flux has not been reported for CuInSe_2 and related alloys. Se, CuCl , InCl_3 and Cu-Se compounds have been evaluated as fluxes for screen-printed CuInSe_2 layers, and non-negligible fluxing reportedly occurs only at relatively high temperatures in Cu-rich material when a liquid Cu_2Se is present. Thus effective fluxing of CuInSe_2 is possible only under conditions that result in Cu-rich CuInSe_2 films unsuitable for solar cells, or in complex multi-step processes such as continuous co-evaporation in which the growing CuInSe_2 film is temporarily made Cu-rich to effect transient fluxing via liquid Cu_2Se before differentially adding In and Se to achieve an In-rich final film composition. Results are also poor when paste mixtures of Cu and In elemental powders are screen printed and overcoated with screen-printed Se powder paste.

Summarizing the prior art, coincident vapor phase processes are difficult to control on large areas; sequential vapor phase processes simplify some of the complexities, but composition uniformity and precursor phase segregation can be severe problems. Metal oxides are useful as phase-stabilized precursors, but uniform, high-rate, vapor phase deposition of oxide solid films is difficult, and spray pyrolysis of oxide solid films is inefficient due to poor materials use efficiencies. Particulate-based processes such as screen printing can have high materials efficiencies, but such processes generally work well only when efficient fluxing processes are available. A clear need exists for phase-stabilized precursors that can be easily converted to thin-film, photovoltaic materials. A need also exists for an easily controlled process for forming such precursors.

It would be especially advantageous to provide a process using particulate precursors to fabricate thin films with well-controlled compositions on large areas, as well as materials and processing techniques for creating high quality, thin film products without contamination from residual flux materials.

BRIEF SUMMARY OF THE INVENTION

The present invention provides unique methods for making phase-stabilized precursors in the form of fine particles, such as sub-micron multinary metal particles, and multi-phase mixed-metal particles comprising at least one metal oxide.

The invention further provides methods of using spraying and coating techniques to deposit thin, close-packed layers of multinary metal and/or mixed-metal metal oxide particles. In one embodiment slurry spraying is used to deposit layers of single-phase, mixed-metal oxide particulates from aqueous slurries sprayed in air on a heated substrate.

In one aspect of the invention, compound materials are formed using precursors comprising multi-phase particles comprising a metal oxide phase. In one embodiment, particulate precursors are deposited as layers on suitable substrates by efficient processes such as slurry spraying. The precursor layers are then converted to useful films by reacting precursor layer components together so as to cause interdiffusion, and/or by reacting the precursor layers with other reactant materials, such as overcoated layers, liquids, vapors or gases, causing ion exchange and interdiffusion. Of particular advantage are multi-phase particles in which each particle contains more than one compositional phase; multi-phase particulate precursors comprising metal oxides yield superior final film characteristics relative to single-phase metal oxide particulate precursors or precursors made up exclusively of non-oxide compound particles.

In another aspect of the invention, the precursors are multi-phase particles comprising both a metal oxide phase and a non-oxide phase. The presence of a non-oxide phase provides advantageous reaction pathways for converting particulate precursor materials to high-quality final materials by, for example, facilitating transient fluxing by intermediate phases during the conversion process. Of particular advantage are multi-phase particles comprising a metal oxide and a metal phase or binary compound phase in which the metal or compound phase facilitates fluxing and densification by forming liquid phases that facilitate transient fluxing between precursor particles during the conversion of the precursor to the final material. The differing conversion rates of the multiple phases of the precursor particles provides a pathway for transient fluxing due to

BRIEF DESCRIPTION OF THE DRAWINGS

Further aspects and details of the invention will become apparent when considered in conjunction with the attached drawings, wherein:

Figure 1 is a schematic representation of the formation sequence of bulk materials in accordance with one method of the present invention; and

Figures 2 and 3 are schematic representations of the formation sequences of films of materials in accordance with alternative methods of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

Throughout the text, the following definitions are used:

- | | | |
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| materials | - | bulk forms, such as free-standing solids or particles, or film forms, such as coatings, layers, or films on a substrate. |
| compound | - | comprising two or more chemically-bonded elements. |
| particulate | - | solid-state, granular pieces; not liquid droplets. |
| precursor | | |
| materials | - | source materials in intermediate bulk or film form that can be subsequently converted to a final desired material. |
| phase | - | a constituent region of specific composition. |
| multi-phase | - | containing more than one phase. |
| mixed-metal | - | containing two or more metals. |
| metal oxide | - | a compound comprising oxygen and at least one metal. |
| non-oxide | - | a chemical moiety substantially devoid of oxygen; or, a chemical moiety in which oxygen is present only as part of a multi-element ion. |
| multinary | - | containing two or more elements. |
| metallic | - | consisting of elemental metals, metalloids, or alloys of elemental metals and/or metalloids, such that the resulting phases(s) is(are) not multinary compound(s). "Metallic" includes, for example, homogeneous particles of a |

single-phase alloy of Cu and In; multi-phase particles containing for example, separate Cu, In and Cu-In alloy phases; and multi-phase particles containing Cu, In, and Se as metals and/or alloys. Excluded are precursors containing stable compounds, such as Cu_xSe , In_xSe and $\text{Cu}_x\text{In}_y\text{Se}$, other than *de minimis* interdiffused layers that may exist, for example, at the interface between a Cu-In metal phase and an adjacent Se metal phase.

The present invention provides processes for forming unique precursor particulate materials, and compound materials made from such precursor materials. The preferred embodiments of this invention are clearly demonstrated in the case of the preparation and processing of CuInSe_2 and related alloys, and relevant illustrative examples are for the most part given below relative to CuInSe_2 , its alloys with Ga and S, and desirable additives such as Na. The considerable advantages of this invention are, however, not limited to these materials; rather, the improvements embodied in this invention are useful for a wide range of bulk and film materials, including but not limited to I-III-VI, II-VI, III-VI, III-V, and II-IV-V compounds and various alloys and dopants of these.

In a first aspect of the invention, a method is provided for making fine particles, such as sub-micron, mixed-metal particles comprising a metal oxide phase or both a metal oxide phase and a non-oxide phase. This first aspect also provides a method for making fine metallic particles, such as sub-micron, multinary, metallic particles.

Particulate materials can be prepared by numerous methods, including laser pyrolysis, atmospheric arc evaporation, solution precipitation, chemical vapor reactions, aerosol pyrolysis, vapor condensation, laser ablation and other such methods as known in the art. Aerosol pyrolysis is particularly useful for low-cost production of mixed-metal particulates comprising metal oxides, and multinary metallic particulates, in particular, substantially solid, substantially spherical particulates. Aerosol pyrolysis is also useful for adding additional desirable constituents such as dopants and alloying elements, such as Ga in CuInSe_2 , and desirable additives, such as Na, in CuInSe_2 and its alloys.

Suitable environments for reacting source materials to form multi-phase mixed-metal particles according to this first embodiment include environments in which a source of energy is present to drive the reaction of source materials to final particulate materials. Such energetic environments include, for example, near-atmospheric-pressure furnaces, vacuum furnaces, microwave furnaces and other such environments as known in the art and capable of heating a material therein. A suitable environment according to this first embodiment is one capable of heating the atomized source materials to a temperature and for a time sufficient for the source materials to react to form the desired final multinary material. Alternatively, if the source material is atomized in such a way as to be inherently highly energetic, such as by being atomized as a molten metal or metal vapor, then the reaction environment need not add any additional energy to the atomized source material. Suitable reaction environments according to this first embodiment include gaseous environments where the ambient pressures are at absolute pressures above, below, or near atmospheric pressure, such as the environment produced in a high-pressure autoclave, a vacuum furnace, and a quartz tube furnace, respectively. A near-atmospheric-pressure, flowing-gas furnace operating at 350° - 1050°C and operated so as to allow 3 or more seconds residence time of sources and reactants in the hot zone is particularly advantageous as a reaction environment for atomized aqueous source solutions.

Suitable ambient gases include oxidizing gases, such as oxygen and air; substantially inert gases such as nitrogen and noble gases; and reducing gases such as hydrogen, hydrogen mixed with inert gases (for example, nitrogen), and hydride gases such as H_2Se , H_2S , etc. Oxidizing ambient gases are particularly advantageous for making oxide final materials; for example, oxygen is advantageous in making single-phase $Cu_2In_2O_5$ particles. Inert ambient gases are particularly advantageous for making multi-phase materials comprising a metal oxide; for example, nitrogen is advantageously employed for reacting aqueous nitrate solutions to make multi-phase $Cu_2O-In_2O_3$ particles in which each particle has localized regions of Cu_2O and In_2O_3 . Reducing ambient gases are particularly advantageous for making multi-phase materials comprising a metal phase

or comprising metal oxide phase and a non-oxide phase; for example, 10 vol% H_2 in N_2 is particularly advantageous for reacting aqueous nitrate solutions to make $Cu-In_2O_3$ metal - metal oxide particulate sources in which each particle comprises a metallic Cu phase and an In_2O_3 oxide phase.

Source materials, ambient gas, and reaction energetics must be controlled to achieve multi-phase particles. For example, single-phase particles of CuO , Cu_2O and Cu can be produced by aerosol pyrolysis of copper nitrate solutions by suitably selecting furnace ambients and operating temperatures. Thus, pyrolysis in nitrogen at $1200^\circ C$ yields Cu_2O ; pyrolysis in nitrogen at $700^\circ C$ yields CuO ; and pyrolysis of comparable source solutions in 7% H_2 in N_2 at $700^\circ C$ yields metallic Cu . By properly choosing source materials, ambient gas and reaction energetics, one can form multi-phase, mixed-metal materials by selecting a pyrolysis process that causes the metal reactants to reach specific degrees of oxidation. For example, a dilute aqueous solution of equal parts copper nitrate and indium nitrate will form single-phase $Cu_2In_2O_5$ when pyrolyzed at about $900^\circ C$ in O_2 , multi-phase $Cu_2O-In_2O_3$ when pyrolyzed at about $900^\circ C$ in N_2 , and multi-phase $Cu-In_2O_3$ when pyrolyzed at about $500^\circ C$ in 10 vol% H_2 in N_2 . Similar results are possible using other source materials such as molten metal droplets and metal vapors. Different mixed metal groupings such as $Zn-Al$, $In-Sn$, etc. will yield single-phase oxides, multi-phase oxides, metal - metal oxide composites, or mixed-metal metallic particles depending on the relative reaction rates and oxidation rates of different metal-containing reactants in the temperature, time and ambient gas characteristics of the reaction environment.

The advantages of this first aspect of the invention are realizable on a wide variety of materials. For example, particulate materials that can be advantageously processed this way include oxide, chalcogenide, metal and hybrid materials such as $Cu_2In_2O_5$, $Cu-In-Se$, $Cu-In$ and $Cu_2Se-In_2O_3$ useful as particulate precursors for forming $CuInSe_2$ and its alloys. Other particulate materials can also be processed according to this embodiment; for example, In_xO-Sn_xO materials for forming indium tin oxide (ITO), $Zn-Al$ materials for forming Al-doped ZnO , $ZnO-CdO$ materials for forming Zn_xCd_yTe , and $Zn_xPyO-ZnO$ materials for forming Zn_xP . These advantages of this first aspect is

particularly evident in Group IIB mixed-metal materials such as ZnO-CdO, Groups IB and IIIB mixed-metal materials such as $\text{Cu}_2\text{In}_2\text{O}_5$, and Groups IIIB and IVB mixed-metal materials such as ITO.

A second aspect of the invention is the use of slurry spraying and meniscus coating methods to deposit particulate layers as precursors for forming thin films.

Particulate precursor layers provide key advantages over solid precursor layers. Solid precursor layers, such as layers of Cu-In and other metal alloys, are subject to inhomogeneities due to phase segregation, e.g. segregation into liquid In and solid Cu-rich Cu_xIn_y phases, at temperatures typically used to convert Cu-In alloys to CuInSe_2 using such conversion pathways as annealing in Se vapor. In contrast, particulate precursors limit the impact of phase segregation by physically constraining a particle's constituents to the dimensions of the particle.

Mixed-metal particles can also improve final composition uniformity control by decoupling sequential constituent addition uniformity from final materials uniformity. For example, in contrast to sputtered or vacuum evaporated Cu and In precursor layers typically used for preparing CuInSe_2 films, which layers generally exhibit spatial variations in Cu/In composition, particulate precursors uniformly containing Cu and In in the desired atomic ratio can preserve the desired CuInSe_2 composition, even when CuInSe_2 film thickness varies due to precursor layer deposition inhomogeneities.

Some of the advantages of particulate, mixed-metal precursors, notably, ease of thin film deposition, can be achieved by using particulates that are substantially composed of the desired final material. However, particles composed of the desired final material often yield inferior film quality. For example, CuInSe_2 particles can be used to form a CuInSe_2 solid or film, but, without effective fluxing (such as by CdCl_2 in CdTe) or special materials formation pathways (such as lower effective melting temperatures for nanoparticles of very small diameters (e.g., 20 nanometers or less)), particulate precursors of the desired final composition, or mixtures of stable compounds of the constituent elements, such as mixtures of Cu_2Se and In_2Se_3 , generally result in final materials with poor cohesion, low density and inferior electronic properties. In contrast, precursors that

undergo chemical and/or structural conversions, such as metallic Cu-In precursors subsequently converted to CuInSe_2 (with an accompanying 2 to 3 times volume expansion), are more likely to yield cohesive, dense CuInSe_2 materials than would comparably processed binary or ternary selenide precursors.

One can also mitigate precursor phase segregation and provide for cohesion and densification by using phase-stabilized precursor materials such as oxides and other compounds. Solid metal oxide precursors such as Cu_2O , In_2O_3 , $\text{Cu}_2\text{In}_2\text{O}_5$ and alloys of these with other compounds are useful in that such oxide phases are more stable against phase segregation at temperatures of 150 - 700°C typically used to convert precursor materials to chalcogenide materials; but solid metal oxide films are difficult to deposit at high rates on large areas. Particulate precursors comprising a metal oxide phase are particularly advantageous in comprising phase-stabilized precursors and in providing for easy and efficient deposition in film form by such low-cost techniques as spraying and printing.

Particulate precursor layers can be deposited by numerous methods. For example, screen printing is widely used to deposit Ag-paste grid lines on silicon solar cells, and screen printing is used to deposit CdTe pastes to fabricate large-area, thin-film solar cells.

Stencil printing, writing and nozzle printing have been used to deposit narrow grid lines of particle-based pastes, and writing and nozzle printing techniques have been used for depositing CdTe layers on large-area substrates. While screen printing, stencil printing, writing and nozzle printing techniques are usable for applications where layer thickness is not critical, such techniques are typically limited to minimum layer thicknesses of 5 to 10 microns. These minimum practical layer thicknesses are substantially larger than the 1 to 2 micron thicknesses typically optimal for thin-film photovoltaics applications, thus these techniques are relatively materials-intensive and costly.

Slurry spraying and meniscus coating methods are advantageous in providing fast, uniform deposition of very thin layers, and the use of such methods to form precursor layers for thin-film photovoltaic films for solar cells is the second aspect of the invention. Slurry spraying methods, such as pneumatic spraying with a pressurized gas nozzle,

hydraulic spraying with a pressurized slurry expelled from through an orifice, ultrasonic spraying with rapidly vibrating atomization surface and electrostatic spraying with a high-voltage electric field to direct the atomized slurry to the part, and meniscus coating methods, such as dip coating in a bath or Langmuir trough, spin coating on a rotating stage, waterfall coating in which the substrate travels through a cascading sheet of slurry, and in-line meniscus coating in which the substrate contacts a slurry pool, are useful for depositing thin, uniform layers of particulate materials on large-area substrates. Such methods are in general not limited by the particle delivery fixturing, such as screen and emulsion thicknesses as in the case of screen printing.

Slurry spraying is particularly advantageous in providing a cost-effective method of depositing thin films on large areas with low capital equipment and indirect materials costs. For example, uniform particle layers of less than 1 micron thickness can be deposited by slurry spraying particles with mean sizes of 0.25 micron or less, and the slurry spray can be rastered to uniformly coat large areas. Slurry spraying can achieve a materials use efficiency of more than 90%.

Slurry spraying can accommodate a wide variety of slurry particles, solvents, additives and spraying conditions to achieve advantageous effects. For example, slurry spraying can accommodate a wide variety of particle types, such as single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ oxides, multi-phase $\text{Cu}_2\text{O-In}_2\text{O}_3$ oxides, multi-phase $\text{Cu-In}_2\text{O}_3$ materials, and metallic Cu-In materials.

Slurry spraying can accommodate a wide variety of solvents, such as water, alcohols, glycols, and mixtures of such solvents. Water is particularly advantageous as a safe and simple slurry solvent into which many types of metal and metal oxide particles will adequately disperse.

Slurry spraying can accommodate a wide variety of slurry additives such as dispersants, thickeners, binders and surfactants to optimize layer properties. A 1 to 5 volume percent of an alcohol such as ethanol is a convenient dispersion aid for aqueous slurries containing metal and/or metal oxide particles, as are various commercial dispersants such as Rohm and Haas Duramax 3002, 3007 and 3019.

Slurry spraying can accommodate a wide degree of solids loading and deposition rates. A solids loading of 0.1 to 200 g/L is preferable for slurry spraying of a water-based slurry of sub-micron metal and/or metal oxide particles. A solids loading of 0.5 to 25 g/L is more preferable and of 5 to 10 g/L is most preferable for 0.1 micron mixed-metal particles comprising a metal oxide.

Slurry spraying can be effected in air or in a controlled environment such as an inert or reducing atmosphere that will mitigate particle oxidation.

Slurry spraying can be effected by a variety of means, including for example by entraining the slurry in a gas flow such as in a pneumatic air brush, by atomizing the slurry from a surface such as in an ultrasonic sprayer, or by expelling the pressurized slurry through a hydraulic nozzle. Pneumatic slurry spraying is particularly advantageous for minimizing spray equipment costs and complexity. Ultrasonic slurry spraying is particularly advantageous for minimizing substrate cooling and slurry losses due to gas flow. Electrostatic slurry spraying is particularly advantageous for maximizing materials use efficiency.

The characteristics of slurry-sprayed layers can be affected by substrate surface temperature. In general it is best if the substrate surface temperature is high enough to vaporize the slurry solvent rapidly enough to avoid slurry pooling and low enough to provide for solvent-facilitated lateral movement of particles on the growing layer surface. Excessively low surface temperatures allows solvent build-up and results in macroscopically non-uniform layers. Excessively high surface temperatures results in the solvent evaporating in flight or too quickly on arriving at the substrate surface and yields microscopic clumping of particles and poor microscopic particle coverage. A heater surface temperature of about 100° - 150°C is advantageous for aqueous slurries.

The advantages of this second aspect of the invention are realizable on a wide variety of materials. One embodiment of this second aspect is spraying an aqueous slurry of single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ particles to form phase-stabilized precursor layers for subsequent conversion into CuInSe_2 . Just as $\text{Cu}_2\text{In}_2\text{O}_5$ particulate layers can be deposited by slurry spraying as precursor layers to form CuInSe_2 , ZnO-CdO particulate layers can

be spray-deposited as precursor layers to form ZnCdTe_2 , and In-Sn-O particulate layers can be spray-deposited as precursor layers to form ITO.

A third aspect of the invention comprises the formation of bulk or film materials from multi-phase, mixed-metal, particulate precursor materials comprising a metal oxide phase.

Referring to Figure 1, this third aspect of the invention is schematically depicted as comprising the step of converting one or more particulate precursor materials 1 to desired bulk materials 2, wherein said precursor materials comprise multi-phase, mixed-metal particles comprising a metal oxide.

Referring to Figure 2, this third aspect of the invention is further depicted as also comprising the steps of (a) depositing one or more precursor layers 3 on a substrate 4 of one or more particulate precursor materials 1, where the precursor materials comprise multi-phase, mixed-metal particles comprising at least one metal oxide, and (b) converting the precursor layers to one or more desired films 5.

Multi-phase, mixed-metal, particulate precursors comprising a metal oxide phase provide key advantages over solid precursors and single-phase particulate precursors.

Fine-grained, single-phase, mixed-metal oxide particulate precursor layers capture many of the advantages of particulate precursor layers comprising oxides, but single-phase particulate precursor layers such as $\text{Cu}_2\text{In}_2\text{O}_5$ converted to films of final materials such as CuInSe_2 by such processes as vapor-phase, gas-phase or solid state reactions with one or more chalcogen-containing materials (such as Se vapor, H_2Se or a Se coating) often yield final materials with low densities and poor electronic qualities, presumably as a result of the precursor particles expanding in diameter upon conversion without coalescing or conforming to fill the voids present prior to conversion. The use, instead, of mixtures of constituent single-phase oxide particulates such as Cu_2O and In_2O_3 can yield somewhat better film cohesion and density due, presumably, to the differing conversion rates and intermediary properties of the different particulate compositions. However, the physical segregation of constituents in separate particles generally requires that thick films be processed for long times at high temperatures to achieve suitable final film composition uniformity. Thick films waste materials and increase costs, and long, high-temperature

processing severely limits the spectrum of suitable substrates and workable solar cell structures.

Multi-phase, mixed-metal, particulate precursors comprising a metal oxide simultaneously provide the advantages of particles, phase-stabilized oxides and multi-material reactions. Thus, two-phase, $\text{Cu}_2\text{O-In}_2\text{O}_3$ particles in which each particle has localized regions of Cu_2O and In_2O_3 can yield thin, CuInSe_2 films comparable in quality to films produced from single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ particles or thicker films produced from mixtures of single-phase binary oxide particles processed for longer times at higher temperatures. Similarly, while both multi-phase $\text{Cu}_2\text{O-In}_2\text{O}_3$ and single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ particulate precursor layers can yield homogeneous CuInSe_2 films when reacted with selenium vapor under suitable conditions, CuInSe_2 films prepared from multi-phase precursors exhibit larger grains and higher densities than do CuInSe_2 films prepared from single-phase precursors using comparable selenization conditions.

The multiple phases of a multi-phase precursor particle can be segregated in any fashion within a particle. For example, phases can be macroscopically segregated within a two-phase particle, as in such idealized cases as where two phases constitute separate hemispheres of a two-phase spherical particle or where one phase forms a concentric shell around a spherical subparticle of the other phase.

Embodiments where one or more phases substantially envelop other phases are particularly advantageous when the outer phases exhibit differing conversion rates and intermediary properties that facilitate improved final material properties. For example, given that a liquid Cu_xSe phase within a CuInSe_2 film can act as a flux to promote grain growth, a precursor comprising $\text{Cu}_2\text{O-In}_2\text{O}_3$ multi-phase particles of Cu_2O around a subparticle core of In_2O_3 should yield the transitory existence of Cu_xSe acting to promote particulate layer cohesion and densification during conversion to the selenide, even for $\text{Cu}_2\text{O-In}_2\text{O}_3$ multi-phase particles that are In-rich overall.

The advantages of multi-phase, particulate precursors containing a metal oxide can also to be realized with mixtures of such precursors with other particulate materials. For example, multi-phase, particulate precursors comprising multiple oxide phases such as

Cu₂O-In₂O₃ can be mixed with other particulates, such as Cu, Cu_xO, Cu_xSe and Se particulates, to facilitate densification and grain growth through fluxing. Such mixtures of particulate precursors can be effected by mechanical mixing of precursor materials before deposition, by co-depositing the multiple precursor materials, or by sequentially depositing the different precursor materials.

The advantages of multi-phase particulate precursors containing a metal oxide can also be realized by combining such precursors with other precursor materials. For example, layers of multi-phase, particulate precursors comprising metal oxide phases, such as In-rich Cu₂O-In₂O₃, can be combined with solid layers of Cu or other metal deposited by physical vapor deposition, solution deposition, and other techniques as known in the art; such composite precursors combining multi-phase, particulate layers and other layers facilitate advantageous reaction pathways, such as Cu_xSe fluxing.

The advantages of this third aspect are realizable on a wide variety of materials. Compound materials that can be processed this way include photovoltaic materials such as CuInSe₂ and its alloys with Ga and S, transparent conductors such as indium tin oxide (ITO), ZnO and ZnO:Al, optoelectronic materials such as Zn_xCd_yTe and Hg_xCd_yTe, and semiconductor materials such as Al_xGa_yAs and Zn_xP.

For example, just as Cu₂O-In₂O₃ multi-phase, particulate precursors are advantageous for forming CuInSe₂, so, too, will In₂O₃-SnO₂, ZnO-CdO and AlO_y-GaO_x particulate precursors be advantageous for forming ITO, Zn_xCd_yTe and Al_xGa_yAs, respectively. Similarly, just as Cu₂O-coated In₂O₃ and In₂O₃-coated Cu₂O particles would be advantageous for forming CuInSe₂, ZnO-coated CdO particles would be advantageous for forming Zn_xCd_yTe. And just as mixtures of Cu₂O-In₂O₃ and Cu particles may yield benefits in forming CuInSe₂, mixtures of ZnO-CdO and Zn particles may yield benefits in forming Zn_xCd_yTe.

A fourth aspect of the invention is the formation of bulk or film materials from multi-phase, mixed-metal, particulate precursor materials comprising both a metal oxide phase and a non-oxide phase.

Referring again to Figure 1, a first step of this aspect of the invention is schematically depicted as the converting of one or more particulate precursor materials 1 to desired bulk materials 2, wherein the precursor materials comprise multi-phase, mixed-metal particles comprising a metal oxide phase and a non-oxide phase.

Referring again to Figure 2, this fourth aspect of the invention is schematically depicted as the steps of (a) depositing one or more precursor layers 3 on a substrate 4 of one or more particulate precursor materials 1, where the precursor materials comprise multi-phase, mixed-metal particles comprising both metal oxide and non-oxide phases, and (b) converting the precursor layers to one or more desired films 5.

Multi-phase, mixed-metal, particulate precursors containing both oxide and metal phases provide particular advantages. For example, $\text{Cu-In}_2\text{O}_3$ particulate precursors in which the particles comprise a metallic Cu phase and an In_2O_3 oxide phase yield differential grain growth, presumably due to Cu_xSe fluxing, given the differential rate of selenization of metallic copper versus the ion exchange conversion of indium oxide to indium selenide, and the solid state diffusion of the binary compounds to form the ternary selenide. As another representative example, $\text{Cu}_2\text{In}_2\text{O}_5\text{-Se}$ multi-phase, particulate precursors incorporate additional constituents into the precursor, simplifying subsequent conversion to the desired final material. Again, separate phases can be segregated in any fashion, with the substantially enveloped structures providing particular advantages.

Multi-phase, mixed-metal, particulate precursors containing both oxide and non-oxide compound phases can also provide other significant advantages. For example, $\text{Cu}_x\text{Se-In}_2\text{O}_3$ particulate precursors provide a direct pathway to Cu_xSe fluxing. Again, separate phases can be segregated in any fashion, with the substantially enveloped structures providing particular advantages.

As with precursors comprising multi-phase, mixed-metal, particulate materials comprising only metal oxide phases, additional advantages accrue with mixtures of particles and with composites with other precursor materials. For example, In-rich $\text{Cu-In}_2\text{O}_3$ particles mixed with Cu and/or Se particles, and layers of $\text{Cu-In}_2\text{O}_3$ particles combined with layers of Se, facilitate Cu_xSe fluxing and/or simple solid state reactions.

particulate precursors limit the impacts of phase segregation common in solid metal precursors.

Multinary, particulate, metal precursor materials can be single-phase or multi-phase materials. For example, Group I and III metals can form single-phase alloys, such as $\text{Cu}_{11}\text{In}_9$, and multi-phase materials, such as regions of pure In within a Cu-rich, Cu-In alloy bulk mass. The multiple phases of a multi-phase, metal precursor can themselves be elemental metals or metal alloys; multi-phase materials include, for example, elemental phases of Cu, In and Se, and alloy phases of Cu-In, Cu-Ga, etc.

The multiple phases of multi-phase, multinary, particulate metal precursor materials can be segregated in any fashion within a particle, including, for example, macroscopically segregated within a particle or as a substantially enveloping coating of one or more phases around inner subparticles of other phases. A particularly preferred case is where one or more phases substantially envelop other phases, for example, Cu on an In subparticle.

Precursor layers of multinary, metal particles can be formed by directly depositing multinary metal particulates by, for example, slurry spraying. Conversely, layers of multinary oxide particles can be deposited and subsequently reduced by, for example, annealing in a reducing environment (such as a hydrogen atmosphere) to form multinary, metal particulate layers.

As with precursors comprising multi-phase, particulate materials comprising metal oxide phases, additional advantages accrue with mixtures of particles and with composites with other precursor materials. For example, In-rich, Cu-In particles mixed with Cu and/or Se particles, and layers of Cu-In particles combined with layers of Se, facilitate Cu_xSe fluxing and/or simple solid state reactions.

The advantages of this fifth aspect of the invention are realizable on a wide variety of materials. For example, just as Cu-In multinary, metal particles are advantageous for forming CuInSe_2 , so, too, In-Sn, Zn-Cd and Zn-Al particles would be advantageous for forming ITO, $\text{Zn}_x\text{Cd}_y\text{Te}$, and Al-doped ZnO, respectively. Similarly, just as In- $\text{Cu}_{11}\text{In}_9$ particles will be advantageous for forming CuInSe_2 , comparable, multi-phase, mixed-metal

composites will be advantageous for other materials. Just as Cu-In particles admixed with Se particles or overcoated with Se will be advantageous for forming CuInSe_2 , Zn-Cd particles admixed with Te particles or overcoated with Te will be advantageous for forming $\text{Zn}_x\text{Cd}_y\text{S}$.

A sixth aspect of the invention is the formation of films from one or more porous precursor layers intercalated with one or more materials. By porous we mean a layer containing void space, such as a layer of particles. By intercalated we mean that the intercalating material partially or substantially fills the voids in the porous layer, such as between the individual particles of a particulate layer. Intercalation is distinct from and distinctly advantageous relative to overcoating, as overcoating generally does not fill the voids with the overcoated material. For example, a Cu-In precursor layer can be overcoated with Se by screen printing, without the Se penetrating into the voids, if any, in the Cu-In precursor layer. This phenomenon is well-known and is used to great advantage in screen printing electrodes on porous and/or pinhole-ridden films where a penetrating overcoating would electrically short-circuit the film. Intercalation purposely seeks to fill the voids, partially or substantially. Another advantage of intercalation is that it facilitates densification and cohesion of films formed from particle-based precursor layers.

Referring to Figure 3, this aspect of the invention comprises depositing one or more precursor layers 12 of one or more porous precursor materials 11 on substrate 9, intercalating the precursor layers with one or more materials 13, and converting said precursor layers to desired films 14.

Intercalated porous precursor layers offer significant advantages over solid precursor layers and unintercalated porous precursor layers. Solid precursor layers, such as Cu-In or layered Cu/In, can be overcoated with reactants, such as Se, to facilitate solid state reactions at temperatures lower than those typically required for vapor-phase or gas-phase reactions. Intercalated particulate precursor layers can provide similar advantages while also providing easier layer deposition and suppressing phase segregation. Unintercalated porous precursor layers can provide the advantages detailed above in the discussion of the second, third, fourth and fifth aspects of the invention;

intercalated porous precursor layers provide additional advantages, including low-temperature conversion and better densification.

Porous precursor layers can be intercalated with one or more materials that provide advantageous processing pathways and/or that provide constituents necessary to form the desired final film composition. The final desired film may be formed by reaction solely between the porous precursor layer and the intercalating materials, or between the intercalated precursor and additional reactants. For example, an oxide precursor layer, such as $\text{Cu}_2\text{In}_2\text{O}_5$, can be intercalated with a metal chalcogen, such as Se, to facilitate a solid state reaction and form a chalcogenide, such as CuInSe_2 . As another example, In-rich $\text{Cu}_2\text{In}_2\text{O}_5$ can be intercalated with a copper-containing material, such as Cu, Cu_2O , or Cu_2Se , to facilitate Cu_xSe fluxing during conversion to CuInSe_2 by reaction with Se vapor. As another example, In_2O_3 can be intercalated with tin or tin oxide, or, conversely, SnO_2 can be intercalated with indium or indium oxide, to facilitate the formation of an indium tin oxide transparent conductor film. Similarly, a particulate layer of ZnO-CdO can be intercalated with Cd, CdO or CdS to facilitate formation of $\text{Zn}_x\text{Cd}_{1-x}\text{S}$.

Porous precursor layers can be intercalated at any time during or after the deposition of the layers. For example, an In-rich $\text{Cu}_2\text{In}_2\text{O}_5$ particulate layer can be intercalated with Cu_xO during deposition of the particulate layer, by hybrid spraying processes in which copper salts are dissolved in an aqueous slurry containing In-rich $\text{Cu}_2\text{In}_2\text{O}_5$, such that spraying onto a heated substrates, in an oxidizing environments simultaneously deposits a layer of $\text{Cu}_2\text{In}_2\text{O}_5$ intercalated with Cu_xO . As another example, In-rich $\text{Cu}_2\text{In}_2\text{O}_5$ can be intercalated with Cu after deposition of the particulate layer, by solution deposition of Cu into the $\text{Cu}_2\text{In}_2\text{O}_5$ layer.

A film can be formed by interdiffusing the constituents of intercalated porous layers or a mixture of intercalated and unintercalated layers. For example, CuInSe_2 can be formed by annealing $\text{Cu}_2\text{In}_2\text{O}_5$ intercalated with Se in a reducing atmosphere so as to cause an ion exchange reaction between oxygen and selenium. Alternatively, intercalated layers can be reacted with additional reactants. For example, In-rich $\text{Cu}_2\text{In}_2\text{O}_5$ particulate layers intercalated with Cu can be reacted with Se vapor or an overcoated Se layer to form

CuInSe₂, and a layer of In-rich Cu₂In₂O₅ particles admixed with Se particles and intercalated with Cu can be interdiffused to form CuInSe₂.

The advantages of this sixth aspect of the invention are realizable on a wide variety of materials. For example, just as In-rich Cu₂In₂O₅ particulate layers intercalated with Cu can be reacted with Se vapor to form CuInSe₂, Zn-rich ZnO-CdO particulate layers intercalated with Cd can be reacted with Te vapor to form ZnCdTe₂.

Certain features of this invention apply to all of the aspects and embodiments described herein. For example, suitable particulate precursor materials as described in the preferred embodiments of this invention can vary in size and shape with precursor form, function and composition. Particulate precursors intended for bulk materials preparation can be of any size, preferably of 1 mm diameter or less, more preferably of 0.1 mm or less. Particulate precursors intended for forming 10 - 100 μm thick films useful for phosphor coatings, acoustic surface wave devices, photodetectors, optical filters, electroluminescent devices and related applications can be of any size less than the desired film thickness, preferably of 5 μm diameter or less, more preferably of 1 μm diameter or less. Particulate precursors intended for forming 0.5 - 10 μm thick films useful for thin-film photovoltaics and related applications can be of any size less than the desired film thickness, preferably of 1 μm or less, more preferably of 0.5 μm or less, most preferably of 0.1 μm or less. Particulate precursor materials of average size less than the ranges specified here may provide equivalent or enhanced results; for example precursor particles of 0.1 μm or less may be used for bulk materials, thick film and thin film applications to advantageous effect.

Particulate precursor materials can be of uniform size, of a broad distribution of sizes, or of specific narrow distributions of sizes. For example, a bulk or thin film material may best be formed by a collection or layer, respectively, of uniformly-sized precursor particles; a thin film material may achieve improved packing density and hence, film density and cohesion, by being formed from a mixture of particulate materials with a range of sizes; and a thin film material may achieve optimal film properties by a specific

distribution of sizes, such as a bimodal distribution of relatively larger, multinary oxide particles mixed with relatively smaller, metal particles.

Particulate precursor particle shape and form can vary with precursor material and preparation method. For example, precursor particles can be spheres, pieces of spheres, plates, irregular solids, and other shapes as may result from various particle formation reactions; and precursor particles can be solid, hollow, spongy, and other forms as may result from various particle formation reactions. Substantially solid, substantially spherical particles are particularly advantageous for achieving densely-packed precursor layers.

Particulate precursor layers can be deposited by numerous methods, including slurry spraying, spray printing, spin coating, meniscus coating, slurry painting, slurry casting, screen printing, stencil printing, writing, nozzle printing, relief printing, intaglio printing, and other such processes as known in the art. Any of these methods is useful to realize the primary advantages of the particulate materials processes disclosed in the third, fourth, fifth and sixth aspects of the invention. Slurry spraying and meniscus coating methods provide unique additional advantages for forming high-quality thin films.

Conversion of precursor layers to desired final films as described in the preferred embodiments of this invention can be effected by numerous methods, including solid-state, vapor-phase, gas-phase and hybrid reactions in, for example, batch or in-line furnaces; liquid-phase reactions in, for example, ion exchange baths; and other such methods and equipment as known in the art. Thermal annealing in a reducing environment is particularly advantageous in providing a simple technique to effect ion exchange and interdiffusion reactions to convert particulate precursors to the desired materials. Temperature and time profiles necessary to cause ion exchange and/or interdiffusion vary with the particular materials being exchanged and/or interdiffused. Typical gas-solid reactions to form CuInSe_2 include a reaction period at approximately 150°C and a high-temperature anneal at approximately 400°C . Solid-state reactions occur at lower temperatures, e.g. about $50^\circ - 75^\circ\text{C}$ lower than typical gas-solid reactions. Vapor-phase reactions can occur at low precursor temperatures, provided that a stable source of reactant vapor is present, e.g., in a vacuum evaporation system. Reactions with

wider-bandgap alloys of CuInSe_2 with Ga and S generally require higher reaction and annealing temperatures, e.g. about $50^\circ - 150^\circ\text{C}$ higher than typical CuInSe_2 reactions. Reactions with oxide-containing precursors generally require higher temperatures than reactions with metal precursors.

Reactants from Group VB, such as P, As, Sb and Bi, and from Group VIB, such as O, S Se and Te, can be present in solid, liquid, vaporous or gaseous forms. For example, $\text{Cu}_2\text{O-In}_2\text{O}_3$ can be reacted with Se to form CuInSe_2 , with Se being present as a solid, such as admixed Se particles, or an overcoated solid or particulate Se layer; as a liquid, such as Se-containing ions in solution; as a vapor, such as Se vapor; or as a gas, such as H_2Se .

Conversion of particulate precursors in powder or layer form to desired final bulk or film materials as described in the preferred embodiments of this invention can be effected by reactions in various environments, including inert atmospheres such as Ar and N_2 ; reducing atmospheres, such as H_2 and gas mixtures containing H_2 ; reactive gas atmospheres, such as atmospheres comprising hydride gases such H_2S and H_2Se ; reactive vapor atmospheres, such as atmospheres comprising one or more metal vapors such as Se_{vap} , S_{vap} and Te_{vap} and such as atmospheres comprising compound vapors such as In_xSe ; reactive liquids; and other such environments as known in the art. Reactive reducing atmospheres comprising a reactive vapor and hydrogen gas are particularly advantageous.

Conversion of particulate precursors to desired final bulk materials as described in the preferred embodiments of this invention can be effected by numerous methods, including vapor-phase and gas-phase reactions in, for example, fluidized bed reactors or calciners; liquid-phase reactions in, for example, stirred reactors; and other such methods as known in the art.

Suitable substrates onto which to deposit precursor layers as described in the preferred embodiments of this invention include any substrate type suitable for the specific application of the final film, including glass, glass coated with substantially transparent conductors such as tin oxide, indium tin oxide and zinc oxide, glass coated with metals such as molybdenum, titanium and tantalum, glass coated with conductive compounds,

glass coated with alkali ion diffusion barrier layers, low-Na glasses, ceramics, metal sheets and foils, polymers, and other such substrates known in the art. Particularly useful are substrates like conductor-coated glass, especially glass coated with molybdenum or conductive metal oxides.

Conversion of precursor layers to desired final films as described in the preferred embodiments of this invention can be effected by numerous methods, including solid-state, vapor-phase, gas-phase and hybrid reactions in, for example, batch or in-line furnaces; liquid-phase reactions in, for example, ion exchange baths; and other such methods and equipment as known in the art. Intercalation of particulate precursor layers as described in the preferred embodiments of this invention can be effected by numerous methods, including spray pyrolysis and hybrid slurry/pyrolysis spraying; solution or chemical bath deposition, electroplating; vapor-phase deposition at precursor layer temperatures below those where substantial reaction between the precursor layer and the vapor occurs; and other such methods as known in the art.

The following nonlimiting examples are illustrative of the invention.

EXAMPLE 1

Single-phase, mixed-metal, $\text{Cu}_2\text{In}_2\text{O}_5$ particulate materials with an average particle diameter of about $0.1 \mu\text{m}$ were prepared by atomizing an aqueous solution containing 0.25 mM each of copper nitrate and indium nitrate in an ultrasonic nebulizer to form a fine aerosol; transporting the aerosol into a quartz tube furnace operated at about 900°C , using oxygen as a carrier gas; and capturing the resulting oxide particulates on a filter membrane at the exit of the furnace.

Particulate average particle diameter is determined by solution concentration and aerosol droplet size; for example, particle diameters of about 0.05 to $0.5 \mu\text{m}$ are formed from ca $5 \mu\text{m}$ droplets by varying the concentration of nitrates in the precursor solution from about 0.015 to 15 milli-Molar. Particulate Cu/In atomic composition ratio is determined for the most part by the relative concentration of nitrates in the precursor

solutions; for example, particle Cu/In ratios of about 0.65 to 1.15 result from substantially equivalent Cu/In ratios in precursor solutions.

EXAMPLE 2

Multi-phase, mixed-metal, $\text{Cu}_2\text{O-In}_2\text{O}_3$ particulate materials were prepared according to Example 1 except that nitrogen was substituted for oxygen as the carrier gas.

EXAMPLE 3

Multi-phase, mixed-metal, Cu-In $_2\text{O}_3$ metallic particulate materials were prepared according to Example 1 except that 10 vol% H_2 in N_2 was substituted for oxygen and the furnace temperature was about 500°C.

Given that metal oxides can be reduced to metals by annealing in suitably reducing atmospheres, it is evident that particles prepared according to this Example except that higher concentrations of H_2 are substituted for 10 vol% H_2 in N_2 will yield multinary, mixed-metal Cu-In particles.

EXAMPLE 4

Single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ particulate materials with an average particle diameter of about 0.1 μm were prepared according to Example 1. Water-based slurries of about 5 to 10 g/L solids loading were prepared by dispersing particulates in de-ionized water using ultrasonic cavitation. Addition of a few weight percent of ethanol and/or a commercial dispersant such as Rohm and Haas Duramax 3002 aided dispersion for some particulate batches. Precursor layers were deposited by spraying the slurries at 1 - 2 mL/min onto heated glass substrates using air or nitrogen as the spraying gas. The resulting $\text{Cu}_2\text{In}_2\text{O}_5$ particulate layers were macroscopically uniform, adhesive and cohesive, and were microscopically uniform with good coverage.

EXAMPLE 5

Multi-phase, mixed-metal, $\text{Cu}_2\text{O-In}_2\text{O}_3$ particulate materials with an average particle diameter of about $0.1\ \mu\text{m}$ were prepared according to Example 2. Precursor layers were spray-deposited using water-based slurries according to Example 4. Precursor-coated substrates were annealed in Se vapor at about 425°C for about one hour in a reducing atmosphere of 7 to 10 vol% H_2 in N_2 to convert the oxide precursor layers to CuInSe_2 films. The grain size of the CuInSe_2 films was examined by electron microscopy and found to be up to 2.5 times larger than the average particle size of the $\text{Cu}_2\text{O-In}_2\text{O}_3$ precursors.

Particulate precursor materials with average particle diameters of 0.06 to $0.5\ \mu\text{m}$ were investigated and found workable, provided that layer thicknesses were at least a few particle diameters.

Slurry solids loadings of about 0.2 to $40\ \text{g/L}$ were investigated and found workable, provided that the substrate temperature and spraying rate were adjusted to mitigate liquid pooling on the substrate surface and solvent evaporation in-flight.

Precursor layers were also deposited with ethanol-based and propylene glycol-based slurries in which the water and dispersant additives were substituted for denatured ethanol and propylene glycol, respectively.

Comparable precursor layers were also deposited by a casting process in which the slurry was applied to the substrates and allowed to air dry.

Comparable results were obtained using bare and tin-oxide-coated glass substrates.

Given that metal oxides can be converted to metal chalcogenides by annealing in the presence of one or more chalcogenides, it is evident that such particulate precursors will be converted into sulfides, tellurides, phosphides, arsenides, antimonides, other such compounds, and alloys of these by substituting or adding, respectively, suitable sources of the appropriate reactants during the conversion process.

EXAMPLE 6

Single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ particulate materials with an average particle diameter of about $0.1 \mu\text{m}$ were prepared according to Example 1. Precursor layers deposited using water-based slurries were prepared according to Example 4 and annealed according to Example 5, yielding CuInSe_2 films with CuInSe_2 grain sizes of at most 1.3 times the average particle size of the $\text{Cu}_2\text{In}_2\text{O}_5$ precursors. The resulting CuInSe_2 films are inferior in density and cohesion relative to comparably processed multi-phase $\text{Cu}_2\text{O-In}_2\text{O}_3$ precursors.

EXAMPLE 7

Multi-phase, mixed-metal, $\text{Cu-In}_2\text{O}_3$ particulate materials with an average particle diameter of about $0.1 \mu\text{m}$ were prepared according to Example 3. Water-based slurries were prepared according to Example 4, and precursor layers were deposited on Mo-coated glass substrates according to Example 5. The precursor-coated substrates were annealed according to Example 4. The grain size of the CuInSe_2 films were examined by electron microscopy and found to be about 2 to 5 times larger than the average particle sizes of the $\text{Cu-In}_2\text{O}_3$ precursors.

Given that multi-phase $\text{Cu-In}_2\text{O}_3$ particulate materials yield significantly larger CuInSe_2 film grain sizes than single-phase $\text{Cu}_2\text{In}_2\text{O}_5$ and multi-phase $\text{Cu}_2\text{O-In}_2\text{O}_3$ particulates, and that multi-phase Cu-In solid layers are reported to yield large CuInSe_2 grains, it is evident that multinary metallic Cu-In particulates prepared according to Example 3 will yield large CuInSe_2 film grains.

EXAMPLE 8

Single-phase $\text{Cu}_2\text{In}_{1.5}\text{Ga}_{0.5}\text{O}_5$ particulate materials with an average particle diameter of about $0.1 \mu\text{m}$ were prepared according to Example 1, except gallium nitrate was substituted for a portion of the indium nitrate. Water-based slurries of $\text{Cu}_2\text{In}_{1.5}\text{Ga}_{0.5}\text{O}_5$ particulate materials were prepared according to Example 4. Precursor layer deposition was carried out according to Example 4, and annealing was carried out according to

Example 5, yielding $\text{CuIn}_{0.75}\text{Ga}_{0.25}\text{Se}_2$ films. Other desirable constituents, such as alloying metals -- for example Al and Ag -- in the CuInSe_2 alloy materials family, and dopant and additive materials -- for example Na, Cd, Zn, P and As -- in the CuInSe_2 alloy materials family, can be incorporated in the desired concentration in a like manner.

Given that alloy constituents, dopants and additive materials can be incorporated into particulate materials by adding sources of the respective alloy constituents, dopants and additive materials to the source solutions to be atomized, it is evident that multi-phase, mixed-metal particles comprising multiple metal oxide phases or both a metal oxide and a non-oxide phase can be prepared with various alloy constituents, dopants and additive materials by adding the appropriate sources of the alloy constituents, dopants and/or additive materials to source solutions prepared and processed according to Examples 2 and 3, respectively. Likewise, it is evident that multinary metallic particles with various alloy constituents, dopants and additive materials can be prepared by appropriately adding to the solutions processed according to Example 3.

EXAMPLE 9

Water-based slurries of about $0.5 \mu\text{m}$ Cu_xO particulate materials where $x \sim 1$ were prepared according to Example 4, and dilute copper nitrate solutions were added to the slurries. Precursor layers of Cu_xO intercalated with Cu_yO where $y \sim 1$ were deposited by spraying these slurry solutions onto heated substrates so as to deposit particles by slurry spraying, and simultaneously by co-depositing Cu_yO by spray pyrolysis so as to partially intercalate the particles. Hybrid slurry/pyrolysis spray deposition of a comparable solution in a suitably reducing atmosphere will yield oxide particles intercalated with Cu metal.

EXAMPLE 10

Water-based slurries of about $0.25 \mu\text{m}$ $\text{Cu}_2\text{In}_2\text{O}_5$ particulate materials were prepared according to Example 4, and dilute copper nitrate solutions were added to the slurries. Precursor layers of $\text{Cu}_2\text{In}_2\text{O}_5$ intercalated with Cu_xO where $x \sim 1$ were deposited

by spraying these slurry solutions onto heated substrates so as to deposit particles by slurry spraying, and simultaneously by co-depositing Cu_xO by spray pyrolysis so as to partially intercalate the particles.

Although this invention is described with respect to a set of preferred aspects and embodiments, modifications thereto will be apparent to those skilled in the art. Therefore, the scope of the invention is to be determined by reference to the claims which follow. Throughout the text and the claims, use of the word "about" in relation to a range of numbers is intended to modify both the low and the high values stated.

WHAT IS CLAIMED IS:

1. A method for making mixed-metal particles, comprising:
preparing a solution selected from the group consisting of a solution comprising two or more dissolved metals and/or metal-containing compounds comprising metals selected from Group IIB, a solution comprising two or more dissolved metals and/or metal-containing compounds comprising at least one each metal selected from Groups IB and IIIB, and a solution comprising two or more dissolved metals and/or metal-containing compounds comprising at least one each metal selected from Groups IIIB and IVB;
forming droplets of the solution; and
heating the droplets to pyrolyze the contents of the droplets to form mixed-metal particles.
2. A method according to claim 1, wherein the mixed-metal particles are a single-phase metal oxide.
3. A method according to claim 1, wherein the mixed-metal particles comprise multiple metal oxide phases.